# Asymmetrical 4x2 Array Microstrip Antenna Using Glass Fiber-Ramie-Alumina-Carbon Composite Substrate for 5G Mobile Communication

Irfan Mujahidin<sup>a</sup>, Budi Basuki Subagio<sup>a</sup>, Muhlasah Novitasari Mara<sup>a,\*</sup>, Helmy<sup>a</sup>, Akio Kitagawa<sup>b</sup>

<sup>a</sup> Department of Telecommunication Engineering, Faculty of Electrical Engineering, Politeknik Negeri Semarang, Semarang, Indonesia <sup>b</sup> Department of Electrical Engineering and Computer Science, Graduate School of Natural Science and Technology, Kanzawa university, Japan Corresponding author: \*muhlasah@polines.ac.id

*Abstract*—This paper proposes an asymmetrical 4x2 array antenna for 5G centimeter-wave (cm-wave) communication systems. To optimize substrate efficiency, we employed a multi-element-antenna array combination using sixteen elements. Our substrate optimization involved a Glass Fiber-Ramie-Alumina Composite with a permittivity of 9.4. The proposed asymmetrical 4x4 array operates within the 3.5 GHz frequency band for 5G cm-wave applications. The individual antenna element achieves a gain of 5.23 dBi, which increases to 10.9 dBi when configured in an eight-element array. The optimized antenna substrate offers several advantages, including improved electrical, mechanical, and chemical properties. This results in a substantial reduction in leakage and attenuation, substantially simplified fabrication processes, and markedly reduced manufacturing costs, making it well-suited for 5G communications. The reduction in manufacturing costs is particularly significant, as it can contribute to overall affordability and widespread adoption of 5G technology. Additionally, the improved electrical and mechanical properties of the substrate ensure reliable and efficient performance in various environmental conditions. Furthermore, the proposed antenna design is compact and lightweight, making it suitable for various applications, including mobile devices, wearable technology, and Internet of Things (IoT) devices. The combination of these advantages positions the proposed antenna as a promising candidate for future 5G communication systems, particularly in scenarios where low-cost, high-performance, compact form factors, efficient power consumption, and robustness against interference are essential.

Keywords— Array microstrip antenna; composite substrate; 5G mobile; glass fiber-ramie-alumina.

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# I. INTRODUCTION

The challenges posed by emerging 5G technology demand antennas with features that can accommodate user terminals as both senders and receivers. Beamforming radiation patterns, for example, are essential for spatial scanning and improved efficiency. Meeting these requirements presents significant design challenges in achieving a reasonable balance between technological design issues and commercial criteria, including low cost, small size, radiation efficiency, antenna gain, broadband performance, and more, especially in the centimeter wave range [1].

It is well-known that higher frequencies lead to smaller antennas, and shorter wavelengths necessitate more antennas for a given coverage area [2], [3]. To realize 6G telecommunications, Principia Scientific International, a nonprofit organization, suggests that communication service operators build base transceiver stations (BTS) at intervals of 100 meters or less. This would require a substantial increase in BTS density [4]. In 2020, MIIT, or the Ministry of Industry and Information of China, declared that more than 690,000 5G base stations are operating in China. This number is still far from the target, considering that another 10 million 5G BTS are needed to cover the entire Chinese region [5], [6]. Similar demands for 5G antennas will likely arise in other countries worldwide.

Among potential solutions, a microstrip antenna with coplanar placement of radiation elements and a power supply network appears promising for 5G applications due to its balance of functionality and manufacturing complexity [7], [8]. However, current methods for increasing the performance and reducing the cost of coplanar antennas remain insufficient.

To reduce costs, currently, most countries use FR4 substrates as microstrip antenna materials. While FR4 offers advantages such as low price, low water absorption, and good insulation, it has limitations in terms of tensile strength and temperature tolerance (up to 130°C) [9], [10]. As the need for microstrip antennas in the extra-high-frequency range grows with the development of next-generation telecommunication systems, reducing dependence on FR4 becomes increasingly important [11], [12]. This paper explores the use of ramie fiber waste as an alternative material to FR4 for the mass manufacture of microstrip antennas. Ramie fiber waste is processed into a Glass Fiber-Ramie-Alumina Composite substrate, which offers advantages in electrical, mechanical, and chemical properties. Glass fiber, which serves as a skeleton, has heat-resistant properties and improves tensile strength and heat resistance to temperature changes [13] Ramie has a high tensile strength [14]. While alumina and carbon have insulated properties and a relative dielectric coefficient value of 10, so if these materials are combined into one into a composite, it will increase the relative dielectric constant of the composite close to pure alumina, from the experiment using VNA the relative dielectric constant of 9.2 is obtained. FR4 has only a dielectric constant value of 4. This material is implemented in a 4x2 antenna array that is designed to address the challenges of microstrip antennas in 5G network communications. The fabricated substrate material is more flexible because the thickness can be changed according to our design to change the capacitance value in the composite with the formula:

$$C = \frac{\varepsilon_0 \varepsilon_r A}{d} \tag{1}$$

where:

C = Proficiency

 $\varepsilon_0$  = Void Dielectric Constant = 8,854 x 10-12 F/m

 $\varepsilon_r$  = Dielectric Constant Relative Material

A = Wide of cross-sectional area

d =Cross-sectional distance

When compared to substrates on the market, for example FR4 and duroid, besides being very expensive, the thickness cannot be changed so that it is difficult to set the parameters.

#### II. MATERIALS AND METHODS

## A. Substrate Composition Design

The manufacturing process commences by sourcing Ramie fiber waste from local Ramie farmers in Wonosobo City. This Ramie fiber waste is then combined with a composite material consisting of Epoxy Resin ( $C_{21}H_{24}O_4$ ), Epoxy Hardener ( $C_6H_{18}N_4$ ), and Alumina powder ( $Al_2O_3$ ) in a 1:1:1 ratio. The procedure involves sequential mixing steps: first, blend the Epoxy Resin and Epoxy Hardener until the color changes [15]. Following this, gradually introduce the Alumina powder and continue stirring until all the ingredients are thoroughly mixed [16]. Subsequently, glass fiber ( $SiO_2$ ) and hemp fiber waste, with cellulose ( $C_6H_{10}O_5$ ) as the primary compound, are coated with the pre-made composite material. This coating enhances the structural integrity and rigidity of the Ramie fiber waste when subjected to pressure on Fig. 1 [17].



Fig. 1 Method for making glass fiber-ramie-alumina composite substrate

The substrate composition design is achieved by arranging the Ramie fiber coated with the composite material on both the upper and lower sides [18], [19]. On the lower side, it is initially protected with a layer of plastic, and after the basting process with the composite material, it is covered with plastic once more. This process serves the purpose of preventing the substrate material from adhering directly to the iron plate when subjected to pressure, facilitating its removal from the mold on Fig. 1 [20], [21].

The subsequent step involves the compression molding of the Ramie fiber, which has been coated with the composite, using two metal plates, as illustrated in Fig. 2. This compression molding process typically spans at least one day.



Fig. 2 High-pressure thick liquid composite coating process

The primary objective at this stage is to validate the suitability of the Ramie-Alumina Composite substrate as an alternative material for replacing FR-4 in the production of microstrip antennas [22], [23]. To achieve this, it is imperative to conduct a comprehensive analysis and measurement of the intrinsic dielectric properties of the Ramie-Alumina Composite substrate during the testing phase [24], [25].

## B. Antenna Design

The microstrip patch antenna's geometry on the glass fiber-Ramie-alumina composite substrate is depicted in Fig. 3. The proposed antenna design encompasses various parameters and specifications. The simulation of the proposed 5G antenna design, utilizing a glass fiber-Ramie-alumina composite substrate, has been conducted. The key parameters assessed during the simulation include return loss, VSWR (Voltage Standing Wave Ratio), radiation pattern, and polarization pattern [26].



Fig. 3 The geometry of microstrip patch antenna on glass fiber-Ramie-alumina composite substrate

The simulated return loss results for the proposed 3.5 GHz 5G antenna design on a glass fiber-Ramie-alumina composite substrate are presented in Figure 4. Through multiple iterations carried out using CST Microwave Studio software, the desired performance target for the antenna was set to achieve a return loss of less than -10 dB [12], [27]. In the case of the asymmetrical 4x4 antenna operating at a frequency of 3.5841 GHz, it achieved a return loss value of -15.494938 dB. The parameter S1,1 is commonly referred to as the return loss in antenna performance analysis.



Fig. 5 The result of the VSWR simulation

The simulation results for VSWR are depicted in Fig. 5. The desired VSWR parameter was set to be less than two, and the simulation results show a value of 1.404584 at the frequency of 3.5841 GHz, as illustrated in Fig. 5.

This indicates that the antenna design on the glass fiber-Ramie-alumina composite substrate meets the VSWR performance requirement. Similarly, the radiation pattern shown in Fig. 6 also meets the performance requirements of antennas implanted in mobile communications with a directional radiation pattern that has a centered HPBW value close to a 0-degree angle.



Fig. 6. The radiation pattern of the proposed antenna in Polar models

To improve the antenna performance, especially the power gain due to the antenna using glass fiber-Ramie-alumina composite substrate for 5G mobile Communication, it is further optimized using the array method with asymmetry aimed at providing wider and wider radiation pattern but increased gain value. The following in Fig. 7 is the result of the optimization process to increase the array antenna, which was originally from a single antenna and then optimized to become a 4x1 array antenna.



Fig. 7 4x1Array Microstrip Antenna Design

The gain obtained after optimization is 5.23 dBi, then optimized again to obtain the most efficient value in terms of radiation pattern, gain, and other performance so that the most optimal dimensions are obtained in Figure 8 so that the gain is 10.9 dBi.



Fig. 8 4x2 Array Microstrip Antenna Design

## III. RESULTS AND DISCUSSION

# A. Glass Fiber-Ramie- Carbon- Alumina Composite Substrates

Relative permittivity or  $\varepsilon_r$  (Epsilon r) is a particularly important parameter in microstrip antenna design. It is the ratio between the dielectric permittivity of a material, such as a glass fiber-Ramie-alumina composite substrate, and the dielectric permittivity of a vacuum. The size of the conductor patch in a microstrip antenna is determined by the relative permittivity value. Evaluating the Alumina - Glass fiber substrate material using a Vector Network Analyzer [28]. The test used a frequency of 3500 MHz with substrate specifications of 3 mm thick, 101.5 cm long, and 110.5 cm wide and found a substrate area of 11215.75 cm<sup>2</sup>. Then, the test results of the relative permittivity of the glass fiber-Ramie-alumina composite substrate material can be obtained Z = 0.69 - 0.43j, based on Equation 2, the test data has a resistance value (R) of 0.69  $\Omega$ and a capacitive reactance value (XC) of -0.43j. Thus, the capacitance value can be obtained with equation 2.

$$\int X_C \, df = \int \frac{1}{2\pi C f} \frac{1}{f} \, df \tag{2}$$

Then to calculate the total capacitive reactance in a substrate volume where the value of *C* is unstable, we can use equation 3. With the initial condition that *C* is a function of the position of the capacitance in three-dimensional space, *C* (x, y, z), and we want to integrate the capacitive reactance  $X_C$  in a substrate volume *V*. Then the equation for the value of  $X_C$  on the substrate volume *V* can be described in equation 3:

$$\iiint X_C \, dV = \, \iiint \frac{1}{\omega^C(x, y, z)} dV \tag{3}$$

Where dV is the infinitesimal substrate volume element. If we use Cartesian coordinates, the substrate volume element dV is dx, dy, dz. The substrate coordinate layer can be described in Fig. 9.



Fig. 9 Composite Layer with tree Dimension coordinate analysis environment

From the capacity value, which is  $C = 2.05730838 \times 10^{-10}$ *F*, the dielectric constant can be obtained by decomposing the characteristic value of the material, which is A area of the substrate plate [29], the thickness of the material is d and  $\varepsilon_0$  is the permittivity of a vacuum then with equation 3 the dielectric constant value of the substrate is 9.419967674  $\approx$  9.4. This is calculated using equation 4 and 5. The dielectric constant will underline an antenna design to determine its dimensions comprehensively. Assuming that (A) and (d) are constant, and then integrating them against the relative permittivity  $\varepsilon_r$  that changes along the substrate medium, it can be decomposed into equation 4.

$$C(\varepsilon_r) = \int \frac{(\varepsilon_0 \times A)}{d} d\varepsilon_r \tag{4}$$

With equation 4, the value of capacitance *C* as a function of relative permittivity  $\varepsilon_r$  can be fulfilled. Then to implement it into a three-dimensional substrate, it is necessary to describe how the phenomenon  $\varepsilon_r$ , *A*, and *d* changes in the space coordinate system. Under the condition that the value of  $\varepsilon_r$  changes as a function of position *x*, *y*, *z*, it can be described by equation 5:

$$C = \iiint \frac{\varepsilon_r \times \varepsilon_r(x,y,z) \times A(x,y,z)}{d(x,y,z)} dV$$
(5)

where V is the calculated antenna substrate volume, and dV is the infinitesimal substrate volume element.

## B. Asymmetrical 4x2 array

In the final stage, the 4x1 antenna array design is copied and translated down as far as the length of the ground and then put together to form a 4x2 antenna array design [30], [31]. Add a parallel connection to connect the two with a length as shown in Figure 10 as a result of the Manufacturing implementation.



Fig. 10 4x2 Array Microstrip Antenna Manufacturing implementation

The given statement describes the final stage of designing a 4x2 antenna array. The design is created by copying and translating the 4x1 antenna array design down to the length of the ground and then connecting the two arrays in parallel. The resulting design is shown in Figure 9 [32], [33], and the specifications of the microstrip antenna array 4x2 design. The search results provide several research papers and articles related to the design of microstrip antenna arrays. These papers discuss the design and development of 4x2 microstrip patch antenna arrays for various applications, such as communication systems. The papers also discuss the optimization of the antenna arrays for increased directivity and circular polarization. Overall, the final stage of designing a 4x2 antenna array involves copying and translating the 4x1 antenna array design and connecting the two arrays in parallel. The resulting design is optimized for increased power gain and ration pattern.

## C. The Result of Antenna Array 4x2

The 4x2 array antenna test result of the return loss parameter for the proposed design and implementation of 3.5 GHz for 5G antenna using a glass fiber-Ramie-alumina composite substrate is shown in Figure 10. The targeted parameter loss achieved for the proposed antenna was less than -10 dB. The antenna 4x2 array works on the frequency 3.5841 GHz and has a value return loss of -39.49 dB.



The tested result of the VSWR parameter is presented in Fig. 11. The targeted parameter of VSWR is less than 2, meanwhile, the tested result gets the value of 1.204584 in the frequency 3.5841 GHz, as shown in Fig. 12.



Fig.12 The tested result of the Radiation Pattern 4x2 Array Antenna

The tested result of the radiation pattern is presented in Fig. 12. The result of the radiation pattern has a main lobe magnitude of 10.9 dBi in frequency 3.5 GHz. From the tests that have been conducted in this study, it can be concluded that the 4x2 array antenna at a frequency of 3.5 GHz is used in 5G communication networks, using a glass fiber-Ramiealumina composite substrate. Overall, the test results showed that the 4x2 array antenna with composite substrate successfully achieves the desired parameters, exhibiting good performance at the frequencies specified for use in 5G communication networks.

## IV. CONCLUSION

In this work, the design of an Asymmetrical 4x2 array antenna for 5G centimeter-wave communication systems is presented. The proposed 5G configuration consists of a multielement-antenna array combination. Each antenna array consists of four elements, which are arranged evenly, but the shape is not symmetrical between the two sides, while the two arrays are then assembled in the same arrangement with different impedance branching. Optimization of the substrate is also conducted by achieving a more efficient substrate was conducted by constructing the structure of the Glass Fiber-Ramie-Alumina Composite compound, which has a er = 9.4. The proposed 5G antenna array covers value of the 3.5 GHz frequency band, which is dedicated to 5G cmwave communication applications. The proposed antenna elements produce a gain of 5.23 dBi, which increased to 10.9 dBi by adopting an eight-element array configuration. By optimizing the antenna design and material substrate, antennas have the advantage of antenna characteristics applied to 5G communications in the form of characters that mutually improve electrical, mechanical, and chemical properties so that they have an extremely high molecular density that makes small leakage. Low losses, easy fabrication, and low manufacturing costs. So, the proposed structure can be a potential candidate for antennas in a more efficient mass 5G communication system. Further research can explore other composite materials by measuring the capacitance value to obtain the value of the relative dielectric constant of the composite material, because the value of the relative dielectric constant is the key so that the antenna can operate at other frequencies.

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